

ZEISS

MMS - Spectral Sensors

An Extended Introduction

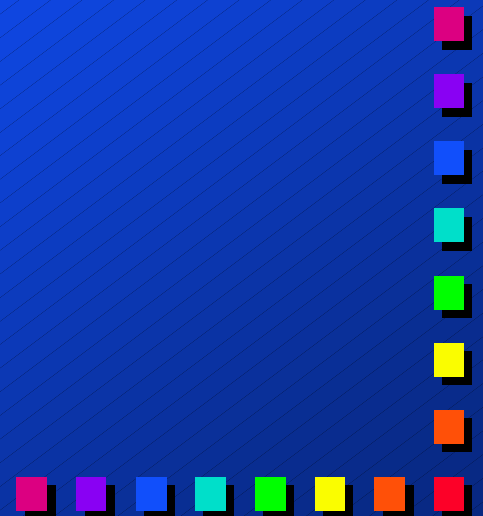


〒100-0001
東京都千代田区千代田千代田第一ビル201号
Tel: 03-5225-2000 Fax: 03-5225-2000



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- Task
- Design and Basics
- Parts
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- Overview of Current Modules
- Driving Electronics
- Forecast

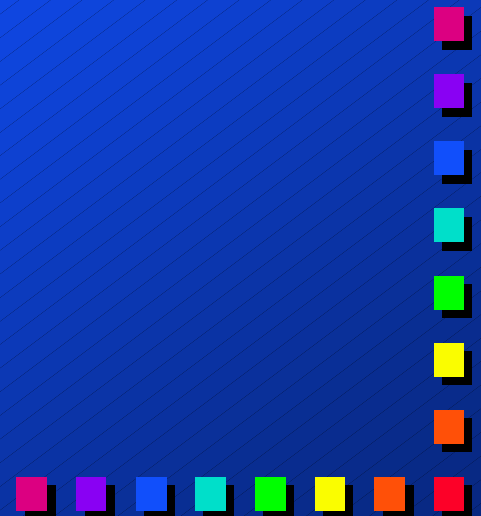


Task

- Fast and reliable collection of complete spectra

obtainable by

- Simultaneous Spectrometers



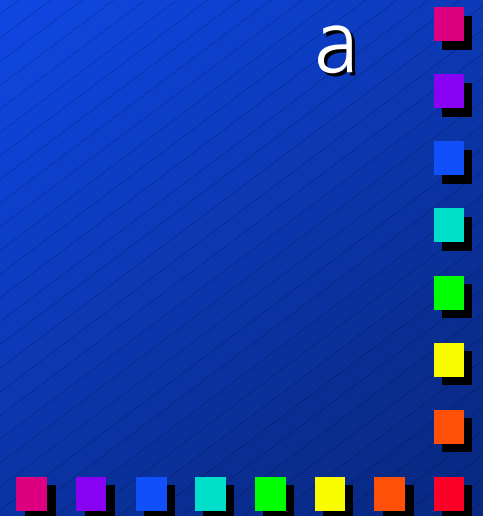
Solution

- Reliable and compact design
- \Rightarrow
- Transformation of a classical spectrometer

into

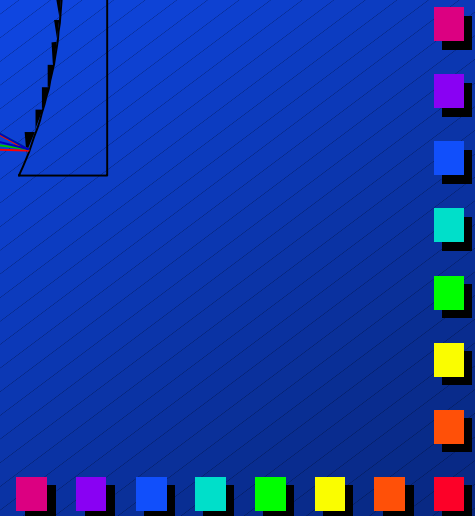
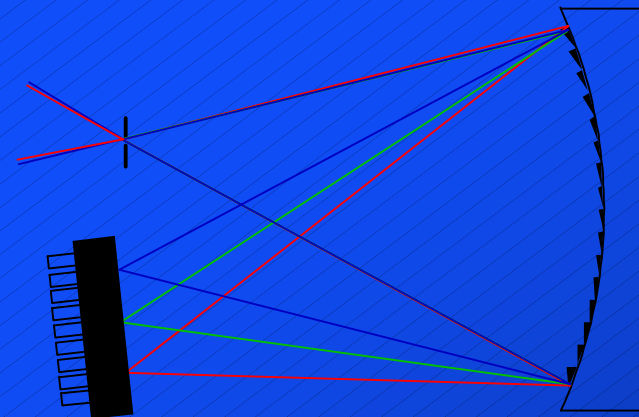
Spectral Sensor

a



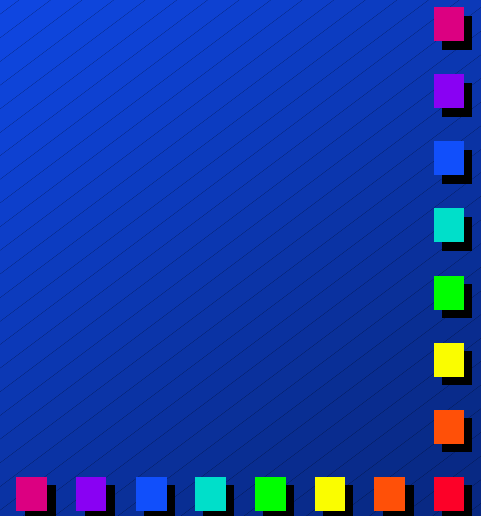
Principal Layout

- Optical Input
- Imaging grating
- Photo diode array



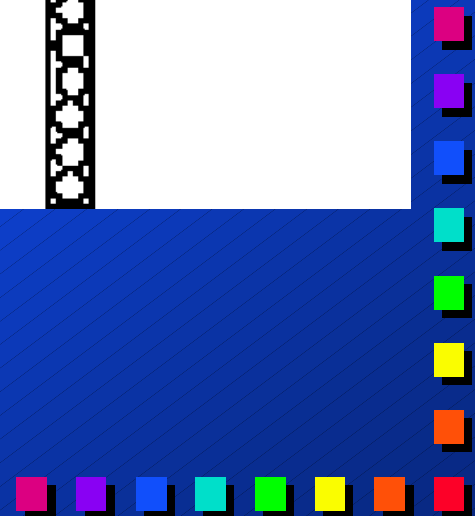
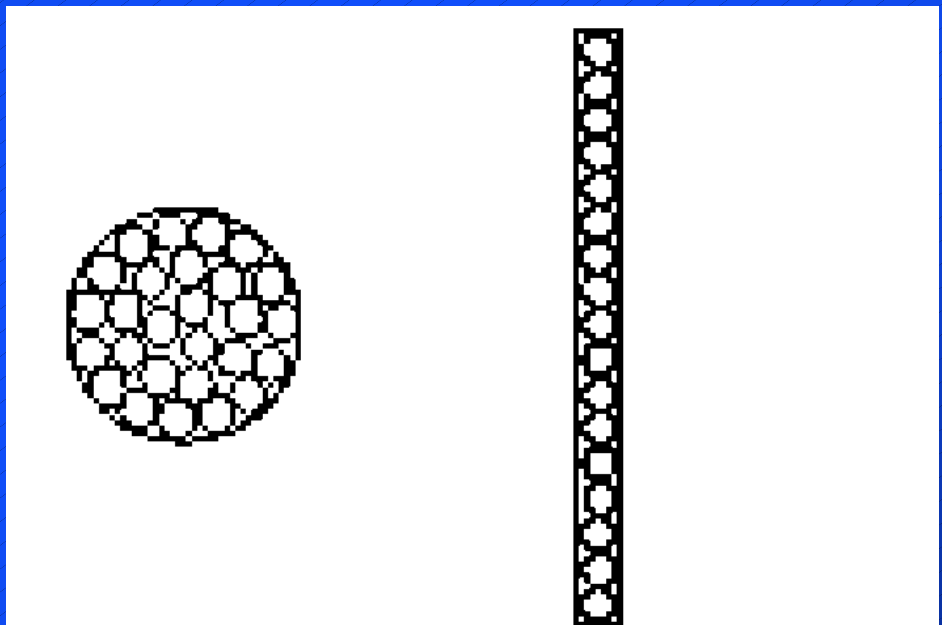
Design Goals

- Reliable, permanently alligned
 - No movable parts
- Fast - Simultaneous read-out
- Sensitive - Optimized light throughput
- Compact



Optical Input

- Fiber cross-section converter
- SMA connector
- $NA = 0.22$
- $\varnothing = 0.5\text{mm}$



Optical Input 2

- Width b_{Slit}
- Height h_{Slit}

- $3 \times b_{\text{Pixel}} \approx b_{\text{Slit}}$
 $= \varnothing_{\text{Fiber}}$

- $h_{\text{Pixel}} = h_{\text{Slit}}$
 $= N_{\text{Fiber}} \times \varnothing_{\text{Fiber}}$

- Effective Area A_{eff}

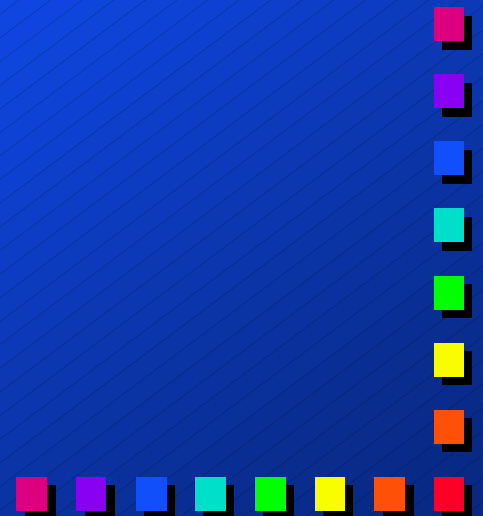
- $A_{\text{eff}} = b_{\text{Slit}} \times h_{\text{Slit}}$

- 1:1 Imaging



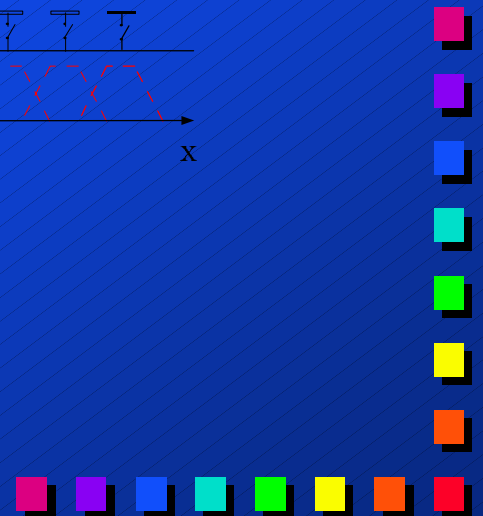
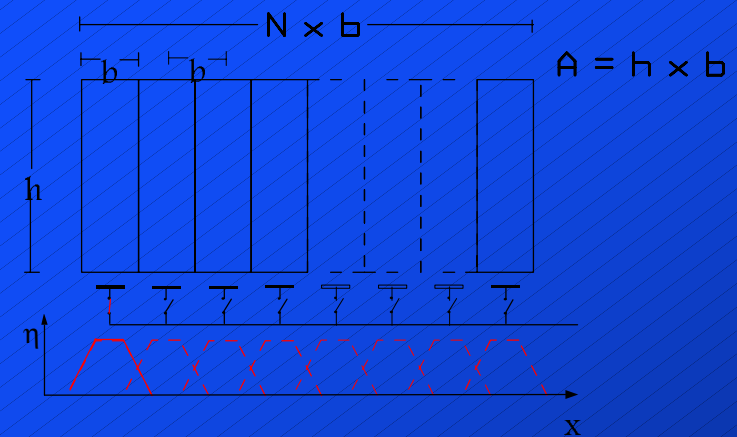
Imaging Grating

- Holographic recording
- Flat-field design
- Imaging corrected
- Blazed = efficiency optimized
- $D/f = (2x) NA_{\text{Fiber}}$



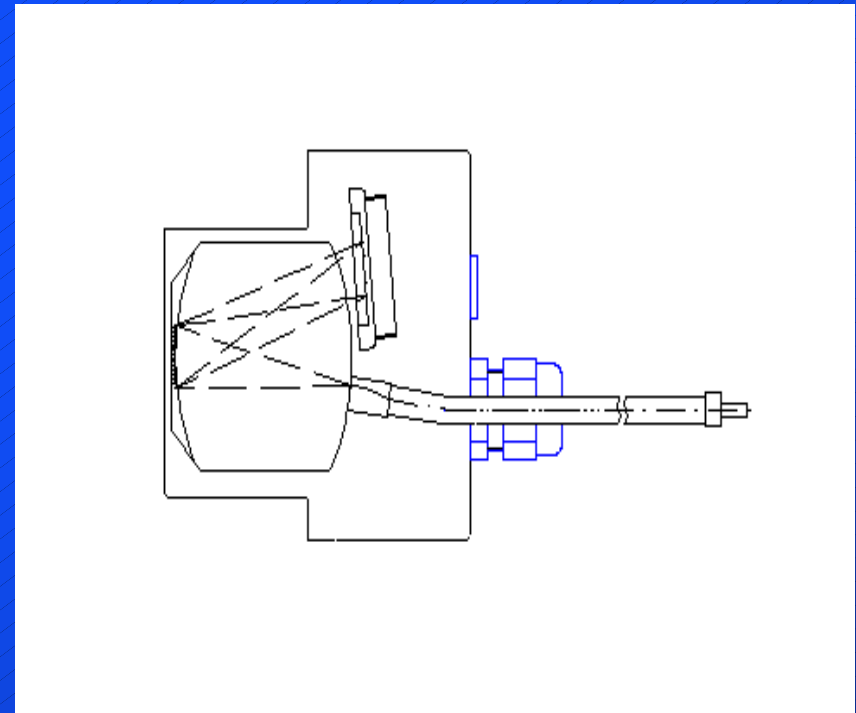
Si Photo Diode Array

- Large pixel area
- 100% fill factor
- Pitch: $25\mu\text{m}$
- Height: $2500\mu\text{m}$
- Number of Pixel:
128 ... 1024
- UV-grad*
 - * NIR enh. quality possible



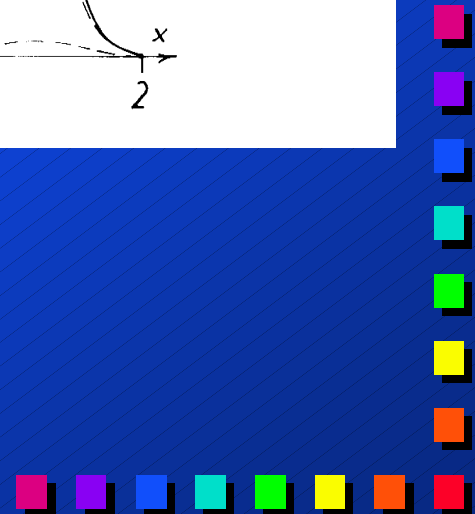
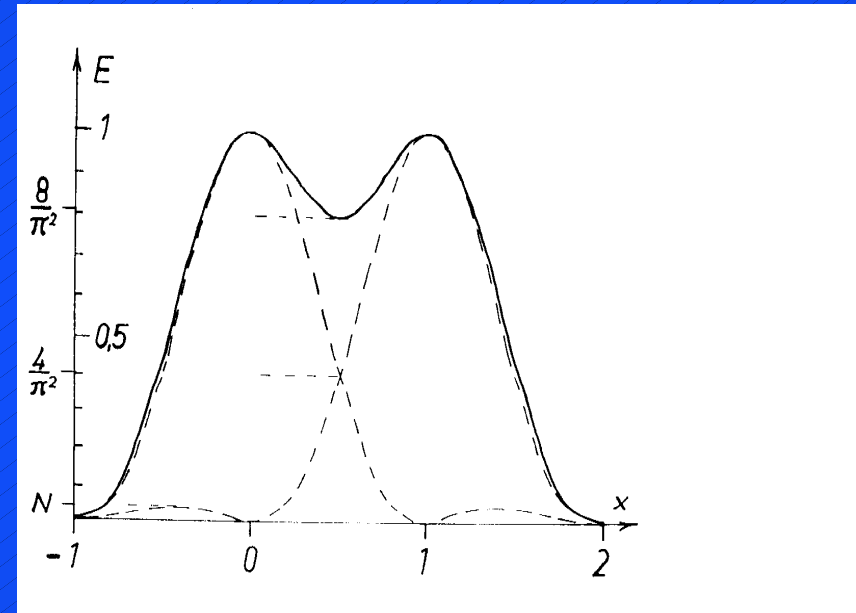
Spectrometer

- All parts glued together
- Integrated preamplifier
- Standard interfaces



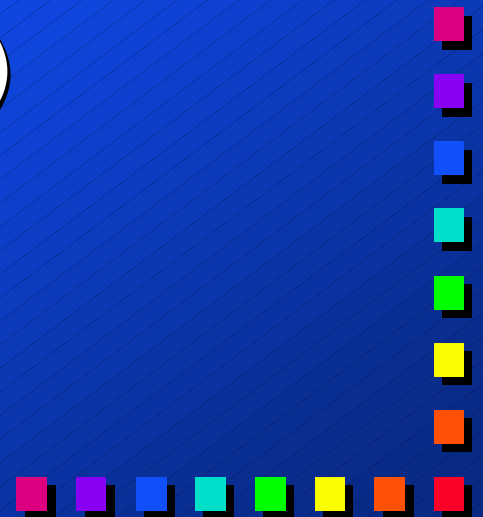
Spectral Resolution

- Rayleigh Criterion
- FWHM
- Bandwidth
- Sub-Pixel Resolution
- Reproducibility



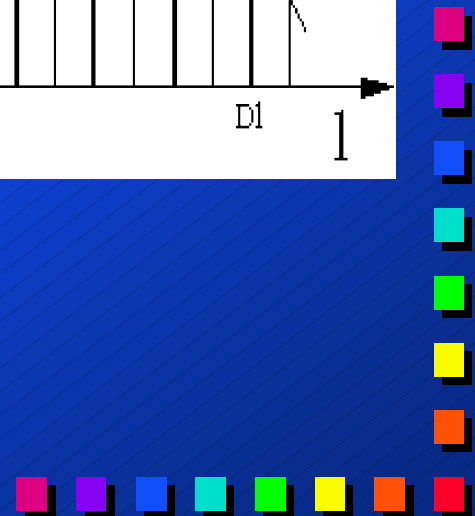
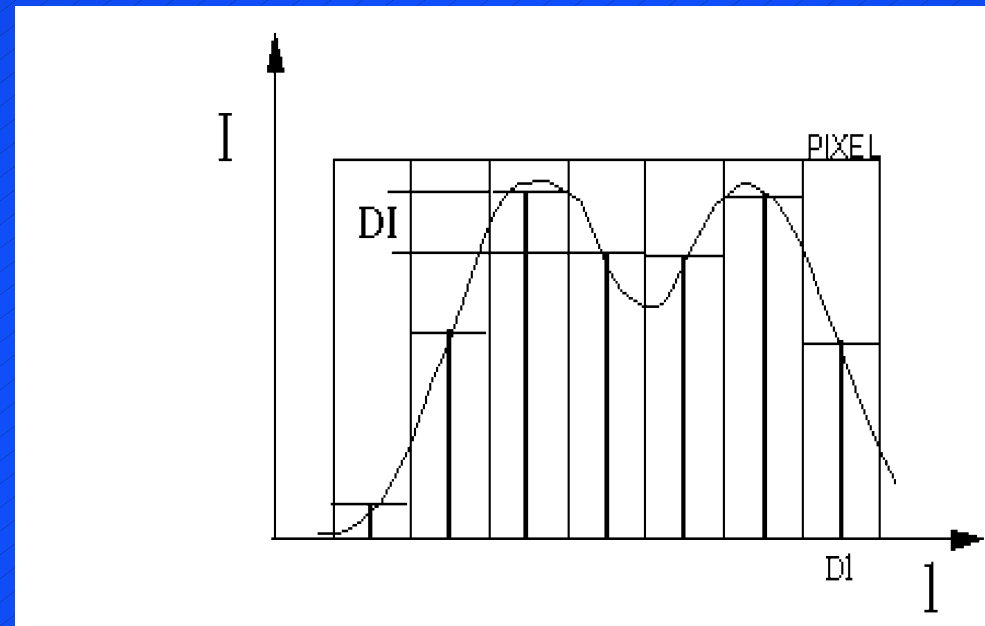
Spectral Resolution DAS

- Rayleigh Criterion
- FWHM \approx
Bandwidth
- Sub-Pixel Res.
- Reproducibility /
Read-Out
Accuracy
- $\Delta\lambda_{\text{Rayl.}} \approx 3 \times \Delta\lambda_{\text{Pixel}}$
- $\Delta\lambda_{\text{FWHM}} \approx$
 $0.9 \times \Delta\lambda_{\text{Rayleigh}}$
- $\Delta\lambda_{\text{SPR}} \approx 0.1 \times \Delta\lambda_{\text{Pixel}}$
- $\Delta\lambda_{\text{abs}}, (\Delta I)$



Rayleigh Criterion DAS

- $\Delta\lambda_{\text{best case}} = 2 \times \Delta\lambda_{\text{Pixel}}$
- $\Delta\lambda_{\text{worst case}} = 3 \times \Delta\lambda_{\text{Pixel}}$



Sub-Pixel Resolution

■ Parabolic Fit: $I(\lambda)$

$$= a \lambda^2 + b \lambda + c$$

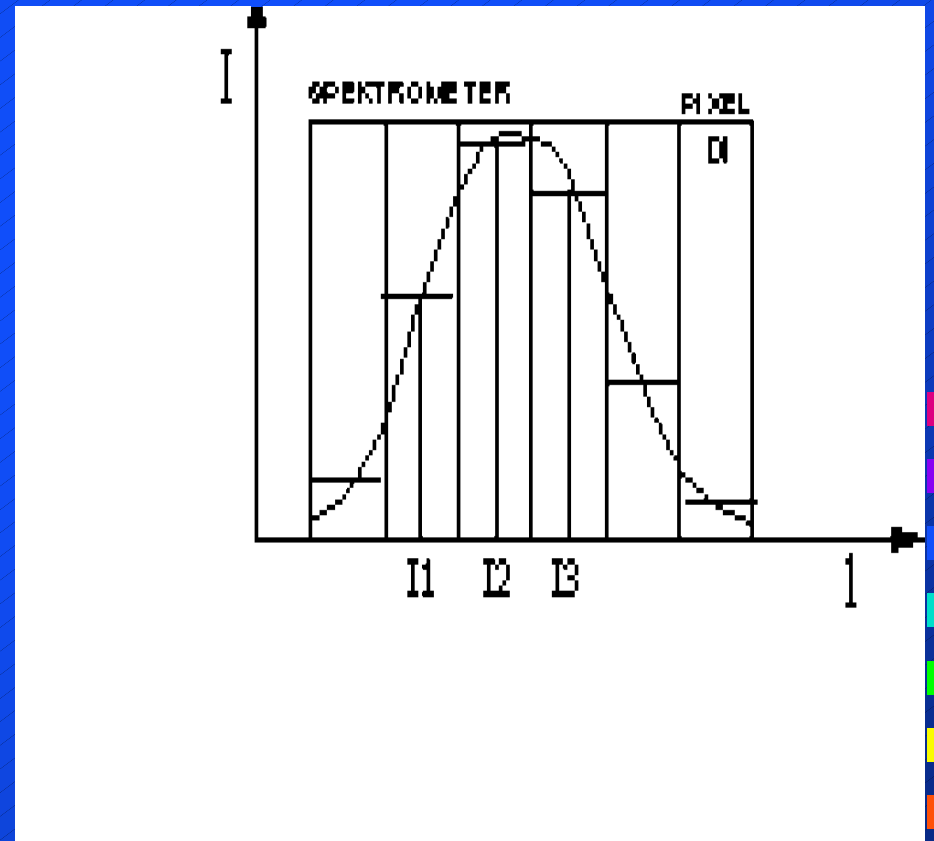
$$\blacksquare a = (I_3 + I_1 - 2I_2) / 2\Delta\lambda^2$$

$$\blacksquare b = (I_3 - I_1) / 2\Delta\lambda - 2a\lambda_2$$

$$\blacksquare c = I_2 - a\lambda_2^2 - b\lambda_2$$

■ $\lambda_{\max} = -b/2a$

■ Fit Procedures for Calibration



Intensity Resolution

- Dynamic Range
- Stability
 - = Stand. Deviation
 - = Noise
 - = Sensitivity
- Dark Current
- Linearity
- Signal / Noise
- $\Delta I = N.E.P.$
- $I_{\text{Dark}} = f(T, t_{\text{int}})$



Intensity Accuracy

■ Dynamic

- Signal / Noise
- ADC
- Sensitivity
- Linearity

- S / N
- $ADC \geq S/N$
- $\Delta I = 1$ Count
- $\Delta L < 1\%$

■ False Light

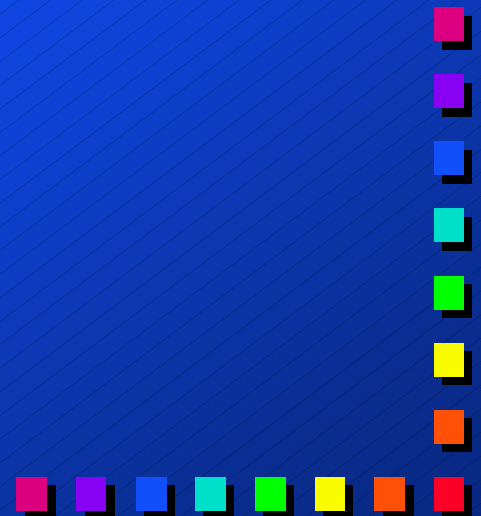
- Straylight
- Other Orders

- Grating is Source
- Blocking Filter
- Structurization



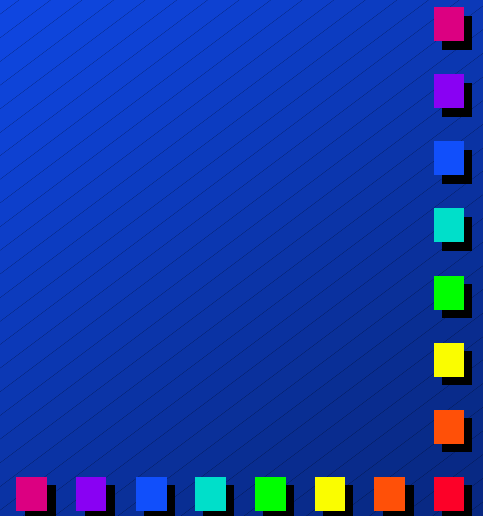
Features

- Robust
- Permantly Calibrated
- High Dynamic Range
- High Light Sensitivity
- High Reproducibility
- Low Temperature Drift



History

- End of 70th
 - Flat-Field-Grating + Dioden Arrays
- 1985 - MCS-Module
- 1993 - MMS 1
- 1995 - MMS UV-VIS
- 1996 - MMS UV
- 1997 - MMS NIR



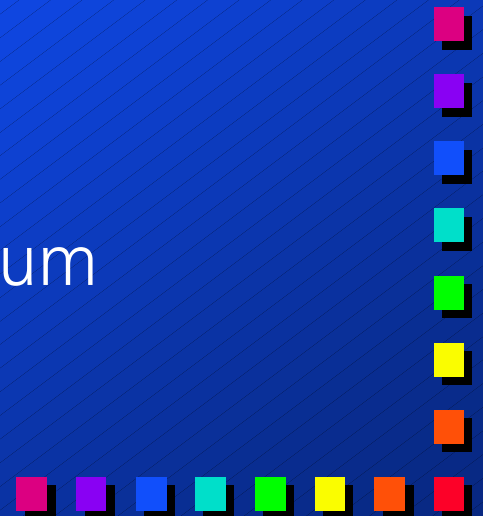
Overview Modules

Name	#Pixels	$\lambda_{\text{Start}}/\text{nm}$	$\lambda_{\text{end}}/\text{nm}$	Resol../nm
MMS 1	256	305	1100	10
MMS UV-VIS	256	190	740	7
MMS UV	256	200	400	3
MMS NIR	128	900	1680	18
MCS UV-NIR	1024	200	1020	2,5
MCS UV-VIS	512	200	620	2,5
MCS VIS	512	360	780	2,5
MCS VIS-NIR	512	680	1100	2,5



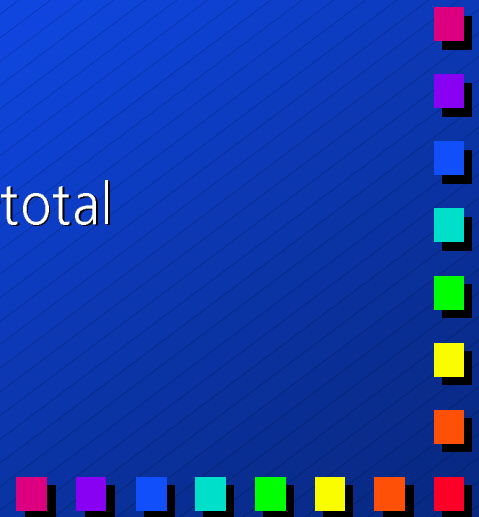
Comparison MMS - MCS

Figure	MMS	MCS
Spectral Range	UV - NIR	UV - IR
Resolution	Low	High
Accuracy	High	Very High
Sensitivity	High	Low
False Light	Moderate	Low
Size/Weight	Small	Medium



Driving

- Clock Rate f_{Clock}
- Integration Time = Exposure Time
- Measurement time
- Measurement Rate (Speed)
- $t_{\text{int,min}} \geq N_{\text{Pixel}} / f_{\text{Clock}}$
- $t_{\text{int,max}}$ limited by I_{Dark}
- $t_{\text{total}} = N_{\text{cycle}} \times t_{\text{int}}$
- $f_{\text{Rate}} = 1/t_{\text{total}}$



Overview Driving Electronics

Figure	CZ 12-Bit	tec 5	CZ MCS
ADC	12 Bit	15 Bit	16 Bit
Noise	1 Count	2 Counts	2 Counts
$t_{int,min}$	10 (5) ms	4ms	3ms
$t_{int,max}$	0.65s	6s	5s
Interface	XT or PCMCIA	AT PC/104	AT or PCMCIA
Multiple Modules	No	4	Cascading Possible



Intensity Accuracy 2

- Signal should be high - Throughput!
- Besides hardware design "intelligent" software design should be applied
- Long-term stability is difficult to check
- Improvement by accumulation of measurements
- Don't forget light source stability!



Forecast

- MMS NIR 2.4 (extended + cooled)
- MMS MIR for Mid-IR-Range
- Low-cost modules
- MCS with higher resolution

